

# Basic equations of flow systems, canonical form, characteristics, 1D unsteady subsonic flow, 2D supersonic steady flow

## 1. Basic flow equations of fluid flow

### Notations:

$\mathbf{w}$  velocity vector

$p$  pressure

$\rho$  density

$T$  absolute temperature

$u$  specific internal energy

$e$  specific total energy  $e = u + \frac{w^2}{2}$

$h$  specific enthalpy

$m$  mass

$\mathbf{I}$  momentum

$\mathbf{F}$  force

$E$  energy

$V$  Volume

$A$  surface, area

$\mathbf{n}$  normal vector of surface

$P$  power

$\dot{Q}$  heat power

Conservation of mass: 
$$\frac{dm}{dt} = \frac{d}{dt} \int_V \rho dV = \int_V \frac{\partial \rho}{\partial t} dV + \int_A \rho \mathbf{w} \cdot \mathbf{n} dA = 0.$$

Conservation of momentum: 
$$\frac{d\mathbf{I}}{dt} = \frac{d}{dt} \int_V \rho \mathbf{w} dV = \int_V \frac{\partial \rho \mathbf{w}}{\partial t} dV + \int_A \rho \mathbf{w} \mathbf{w} \cdot \mathbf{n} dA = \mathbf{F}_{body} + \mathbf{F}_{surface}.$$

Conservation of energy: 
$$\frac{dE}{dt} = \frac{d}{dt} \int_V \rho e dV + \int_A \rho e \mathbf{w} \cdot \mathbf{n} dA = P_{body} + P_{surface} + \dot{Q}.$$

By neglecting surface friction surface forces result from pressure distribution on channel walls.

$$\mathbf{F}_{pressure} = - \int_A p \cdot \mathbf{n} dA.$$

Its power is

$$P_{pressure} = - \int_A p \mathbf{w} \cdot \mathbf{n} dA.$$

Let's write these equations for a channel with cross section  $A = A(x)$  varying along the  $x$  axis. The area  $A$  doesn't change in time. Velocity  $\mathbf{w}$  – average velocity– is parallel to the normal vector  $\mathbf{n}$  of channel cross section  $A$ , thus  $\mathbf{w} \cdot \mathbf{n} = w$ .

Body forces will be neglected; surface forces will be identified with pressure force. The above equations are integrated on an elementary volume  $dV = A dx$ . We get three conservation equations in the above order.

Conservation of mass: 
$$\frac{\partial(\rho A)}{\partial t} + \frac{\partial(\rho A w)}{\partial x} = 0,$$

Conservation of momentum: 
$$\frac{\partial(\rho A w)}{\partial t} + \frac{\partial A(\rho w^2 + p)}{\partial x} = p \frac{dA}{dx},$$

Conservation of energy: 
$$\frac{\partial(\rho e A)}{\partial t} + \frac{\partial(\rho w e + p w) A}{\partial x} = \dot{Q}.$$

These equations can be written in the concise form  $\frac{\partial \mathbf{U}}{\partial t} + \frac{\partial \Phi}{\partial x} = \mathbf{S}$ , where

$$\mathbf{U} = \begin{pmatrix} \rho A \\ \rho w A \\ \rho e A \end{pmatrix}, \quad \Phi = \begin{pmatrix} \rho w A \\ (\rho w^2 + p) A \\ (\rho w e + p w) A \end{pmatrix}, \quad \mathbf{S} = \begin{pmatrix} 0 \\ p \frac{dA}{dx} \\ \dot{Q} \end{pmatrix}.$$

Some numerical codes use this style as fluxes  $\Phi$  are defined on the boundaries of elementary cells, e.g. hexahedra's while elements of  $\mathbf{U}$  are defined in the centres of cells when integrating the conservation equations on a cell having a finite volume.

Through a lengthy computation one dimensional equations can be transformed into non-conservation form if e.g. conservation of mass is substituted into conservation of momentum after differentiating product-terms. We get finally

Conservation of mass:  $\frac{\partial \rho}{\partial t} + \rho \frac{\partial w}{\partial x} + w \frac{\partial \rho}{\partial x} = -\frac{\rho w^2}{A} \frac{dA}{dx},$  (\*)

Conservation of momentum:  $\frac{\partial w}{\partial t} + \frac{1}{\rho} \frac{\partial p}{\partial x} + w \frac{\partial w}{\partial x} = 0,$  (\*\*)

Conservation of energy:  $\frac{\partial p}{\partial t} + w \frac{\partial p}{\partial x} + \rho c^2 \frac{\partial w}{\partial x} = \dot{Q} - \frac{\rho w c^2}{A} \frac{dA}{dx}.$

Speed of sound has been denoted by  $c$  in the last equation defined by  $c^2 = \frac{dp}{d\rho} = \kappa R T = \kappa \frac{p}{\rho}.$

We can summarize the three basic laws again this time in vector-matrix form:

$$\frac{\partial \mathbf{V}}{\partial t} + \mathbf{M} \frac{\partial \mathbf{V}}{\partial x} = \mathbf{S}.$$

Actually

$$\frac{\partial}{\partial t} \begin{pmatrix} \rho \\ w \\ p \end{pmatrix} + \begin{pmatrix} w & \rho & 0 \\ 0 & w & 1 \\ 0 & \rho c^2 & w \end{pmatrix} \cdot \frac{\partial}{\partial x} \begin{pmatrix} \rho \\ w \\ p \end{pmatrix} = \begin{pmatrix} -\frac{\rho w^2}{A} \frac{dA}{dx} \\ 0 \\ \dot{Q} - \frac{\rho w c^2}{A} \frac{dA}{dx} \end{pmatrix}. \quad (***)$$

The second term is the product of a matrix and a vector. Eigenvalues of matrix

$\mathbf{M} = \begin{pmatrix} w & \rho & 0 \\ 0 & w & 1 \\ 0 & \rho c^2 & w \end{pmatrix}$  play an important role with respect to existence of solutions of the equation

system. The eigenvectors  $\mathbf{e}_i$  are solutions of the homogenous algebraic equation  $(\mathbf{M} - \lambda_i \mathbf{E})\mathbf{e}_i = 0$  where  $\mathbf{E}$  is the unite matrix. In order that a solution exists  $\det(\mathbf{M} - \lambda \mathbf{E}) = 0$  must be valid. In details

$$\det \begin{vmatrix} w - \lambda & \rho & 0 \\ 0 & w - \lambda & 1 \\ 0 & \rho c^2 & w - \lambda \end{vmatrix} = 0, \text{ or } (w - \lambda) \left[ (w - \lambda)^2 - c^2 \right] = 0.$$

It can be seen that the three eigenvalues are

$$\begin{aligned}\lambda_1 &= w, \\ \lambda_2 &= w + c, \\ \lambda_3 &= w - c.\end{aligned}$$

The importance of these eigenvalues are obvious if we want to describe the unsteady isentropic flow of an ideal gas through a pipe of constant cross section. In this case equations (\*) and (\*\*) are

$$\frac{\partial \rho}{\partial t} + \rho \frac{\partial w}{\partial x} + w \frac{\partial \rho}{\partial x} = \frac{\partial p}{\partial t} + w \frac{\partial p}{\partial x} + \rho c^2 \frac{\partial w}{\partial x} = 0 \quad (1)$$

$$\frac{\partial w}{\partial t} + \frac{1}{\rho} \frac{\partial p}{\partial x} + w \frac{\partial w}{\partial x} = 0 \quad (2)$$

we have introduced the square of sound velocity  $c$  in equation (\*) giving the second form of (1).

Differentiating (1) with respect to  $t$  and (2) with respect to  $x$  then substituting  $\frac{\partial^2 w}{\partial x^2}$  from the  $x$ -derivative of equation (1) we get a second order partial differential equation (PDE) for the unknown  $p$ . In this new equation only first order partial derivatives of the dependent variables stand beside the second partial derivatives of  $p$ :

$$(w^2 - c^2) \frac{\partial^2 p}{\partial x^2} + 2w \frac{\partial^2 p}{\partial x \partial t} + \frac{\partial^2 p}{\partial t^2} = F\left(w, \frac{\partial w}{\partial t}, \frac{\partial w}{\partial x}, \frac{\partial p}{\partial x}\right). \quad (3)$$

The above equation can be written in general form

$$a(x,t) \frac{\partial^2 p}{\partial x^2} + 2b(x,t) \frac{\partial^2 p}{\partial x \partial t} + c(x,t) \frac{\partial^2 p}{\partial t^2} = F(\text{lower order terms}). \quad (3^*)$$

## 2. The type of the 2<sup>nd</sup> order PDE, canonical form

Equation (3<sup>\*</sup>) is called a **second order PDE** for the unknown  $p(x,t)$  **quasilinear in its main part**. The terms containing second order derivatives are called the main part. Coefficients  $a, b, c$  of the second order partial derivatives can be arranged into a symmetric matrix. This matrix has the form

in the general case (3<sup>\*</sup>)  $\mathbf{A} = \begin{pmatrix} a(x,t) & b(x,t) \\ b(x,t) & c(x,t) \end{pmatrix}$  and in the special case (3)  $\mathbf{A} = \begin{pmatrix} w^2 - c^2 & w \\ w & 1 \end{pmatrix}$ .

The type of the PDE is determined by the **sign** of the determinant  $\det(\mathbf{A}) = a(x,t)c(x,t) - b^2(x,t)$  of matrix  $\mathbf{A}$ .

- If  $\det(\mathbf{A}) > 0$ , **definite**, the type of the PDE is **elliptic**,
- if  $\det(\mathbf{A}) = 0$ , **semidefinite**, the type of the PDE is **parabolic**,
- if  $\det(\mathbf{A}) < 0$ , **indefinite**, the type of the PDE is **hyperbolic**.

Let's transform the independent variables  $x, t$  through the functions  $\xi = \xi(x, t)$ ,  $\eta = \eta(x, t)$  leading to a simpler form of the equation. We suppose that  $\xi$  and  $\eta$  are continuously differentiable functions thus the Jacobian must be **nonzero**,  $J = \frac{\partial(\xi, \eta)}{\partial(x, t)} \neq 0$ . By applying the chain rule:

$$\frac{\partial}{\partial x} = \frac{\partial}{\partial \xi} \xi_x + \frac{\partial}{\partial \eta} \eta_x \quad ; \quad \frac{\partial}{\partial t} = \frac{\partial}{\partial \xi} \xi_t + \frac{\partial}{\partial \eta} \eta_t,$$

further

$$\begin{aligned} \frac{\partial^2}{\partial x^2} &= \left( \frac{\partial^2}{\partial \xi^2} \xi_x + \frac{\partial^2}{\partial \xi \partial \eta} \eta_x \right) \xi_x + \frac{\partial}{\partial \xi} \xi_{xx} + \left( \frac{\partial^2}{\partial \eta \partial \xi} \xi_x + \frac{\partial^2}{\partial \eta^2} \eta_x \right) \eta_x + \frac{\partial}{\partial \eta} \eta_{xx} = \\ &= \frac{\partial^2}{\partial \xi^2} \xi_x^2 + 2 \frac{\partial^2}{\partial \xi \partial \eta} \xi_x \eta_x + \frac{\partial^2}{\partial \eta^2} \eta_x^2 + \xi_{xx} \frac{\partial}{\partial \xi} + \eta_{xx} \frac{\partial}{\partial \eta}. \end{aligned}$$

Similarly

$$\frac{\partial^2}{\partial x \partial t} = \frac{\partial^2}{\partial \xi^2} \xi_x \xi_t + \frac{\partial^2}{\partial \xi \partial \eta} (\xi_x \eta_t + \eta_x \xi_t) + \frac{\partial^2}{\partial \eta^2} \eta_x \eta_t + \dots,$$

and

$$\frac{\partial^2}{\partial t^2} = \frac{\partial^2}{\partial \xi^2} \xi_t^2 + 2 \frac{\partial^2}{\partial \xi \partial \eta} \xi_t \eta_t + \frac{\partial^2}{\partial \eta^2} \eta_t^2 + \dots$$

Putting these derivatives into the left hand side of Eq. (3\*) the second order terms will be

$$\begin{aligned} &\left( a(x, t) \xi_x^2 + 2b(x, t) \xi_x \xi_t + c(x, t) \xi_t^2 \right) \frac{\partial^2}{\partial \xi^2} + \\ &+ 2 \left( a(x, t) \xi_x \eta_x + b(x, t) (\xi_x \eta_t + \eta_x \xi_t) + c(x, t) \xi_t \eta_t \right) \frac{\partial^2}{\partial \xi \partial \eta} + \\ &+ \left( a(x, t) \eta_x^2 + 2b(x, t) \eta_x \eta_t + c(x, t) \eta_t^2 \right) \frac{\partial^2}{\partial \eta^2} = \dots \quad (4^*) \end{aligned}$$

The coefficients of the first and third term have the same structure with the only difference that the coefficient in the first term contains derivatives of the new variable  $\xi$  while the third term derivatives of  $\eta$ . When equating the coefficients of the first and third term in Eq. (4) with zero only the middle term remains.

$$\begin{aligned} a(x, t) \xi_x^2 + 2b(x, t) \xi_x \xi_t + c(x, t) \xi_t^2 &\stackrel{!}{=} 0, \\ a(x, t) \eta_x^2 + 2b(x, t) \eta_x \eta_t + c(x, t) \eta_t^2 &\stackrel{!}{=} 0 \end{aligned} \quad (5^*)$$

From the first equation

$$\xi_t = \frac{-2b(x, t) \xi_x \pm \sqrt{4b^2(x, t) \xi_x^2 - 4c(x, t) a(x, t) \xi_x^2}}{2c(x, t)} = \frac{-b(x, t) \pm \sqrt{-\det(\mathbf{A})}}{c(x, t)} \xi_x.$$

The difference equation of a  $\xi(x, t) = \text{constant}$  level as the change (total derivative) of  $\xi$  along such a line is zero:

$$d\xi = \xi_x dx + \xi_t dt = 0, \quad \text{or} \quad \xi_t = -\frac{dx}{dt} \xi_x.$$

By comparing the last two equations one can see that the slope of a  $\xi(x,t) = \text{constant}$  line is

$$\frac{dx}{dt} = \frac{b(x,t) \mp \sqrt{-\det(\mathbf{A})}}{c(x,t)}.$$

This equation has

- two real solutions if  $\det(\mathbf{A}) < 0$  thus for hyperbolic equations,
- one real solution if  $\det(\mathbf{A}) = 0$  thus for parabolic equations and
- no real solutions if  $\det(\mathbf{A}) > 0$  thus for elliptic equations.

These characteristics had been found by transforming the 2<sup>nd</sup> order PDE into its “**canonical form**”. The transformation was executed on the independent variables.

In the special case (3) the value of the determinant  $\det(\mathbf{A}) = (w^2 - c^2) \cdot 1 - w \cdot w = -c^2$  is negative our equation (3) is of **hyperbolic type**.

As we see; wave equation is typically hyperbolic.

The equation of heat conduction or of 2D diffusion  $(\frac{\partial C}{\partial t} - \alpha(\frac{\partial^2 C}{\partial x^2} + \frac{\partial^2 C}{\partial y^2})) = -u \frac{\partial C}{\partial x} - v \frac{\partial C}{\partial y}$  is parabolic,

2D vortex free flow of an incompressible fluid  $(\frac{\partial^2 \Phi}{\partial x^2} + \frac{\partial^2 \Phi}{\partial y^2} = 0)$  or an electromagnetic field is elliptic.

Equations (5\*) related to the special case are

$$\begin{aligned} (w^2 - c^2)\xi_x^2 + 2w\xi_x\xi_t + \xi_t^2 &= 0, \\ (w^2 - c^2)\eta_x^2 + 2w\eta_x\eta_t + \eta_t^2 &= 0 \end{aligned} \quad (5)$$

From the first equation

$$\frac{dx}{dt} = w \mp \sqrt{-\det(\mathbf{A})} = w \mp c.$$

The characteristic differential equation will disintegrate into a pair of two simple equations

$$\frac{dx}{dt} = w \pm c. \quad (6)$$

The solutions of (6) are:

$$\begin{aligned} x &= (w + c)t + \xi \\ x &= (w - c)t + \eta \end{aligned}$$

where rearranging for the integration constants  $\xi$  and  $\eta$  give

$$\begin{aligned} \xi &= x - (w + c)t, \\ \eta &= x - (w - c)t. \end{aligned}$$

**The slopes of the two series of characteristic lines:**  $\xi = \text{constant}$ , and  $\eta = \text{constant}$  on the  $t - x$  plane **is identical with the eigenvalues of matrix  $\mathbf{M}$ , but NOT of  $\mathbf{A}$ !!!**

After having found the transformation simplifying the main part of the 2<sup>nd</sup> order PDE we can calculate this transformed main part.

The coefficient of the derivative  $\frac{\partial^2 p}{\partial \xi \partial \eta}$  in formula (4\*) will be  $2 \left( a(x,t) - \frac{b^2(x,t)}{c(x,t)} \right) \xi_x \eta_x$

and in the special case (4) this coefficient is  $-4c^2$  thus the simple main part is

$$-4c^2 \frac{\partial^2 p}{\partial \xi \partial \eta} = \dots,$$

this is the canonical form of the PDE, its type is **hyperbolic**.

Through a second transformation  $\psi = \xi + \eta$ ,  $\varphi = \xi - \eta$  we get the other canonical form of hyperbolic 2<sup>nd</sup> order PDE's:  $\frac{\partial^2 p}{\partial \xi \partial \eta} = \frac{\partial^2 p}{\partial \psi^2} - \frac{\partial^2 p}{\partial \varphi^2} = \dots$ .

### **Method of characteristics (MOC); the form of ODE's to be solved along the characteristics**

Let's add Eq.(1) to the  $\rho c$ -times of Eq. (2) then push the term  $\rho c$  into the derivatives of  $w$ ! We receive  $\frac{\partial p}{\partial t} + \rho w c \frac{\partial w}{\partial t} + c \frac{\partial p}{\partial x} + c \frac{\partial \rho c w}{\partial x} + w \frac{\partial p}{\partial x} + w \frac{\partial \rho c w}{\partial x} = 0$ . This can be written in a denser form:

$\frac{\partial}{\partial t}(p + \rho w c) + (w + c) \frac{\partial}{\partial x}(p + \rho c w) = 0$ . Remembering that Eq. (6) with the upper sign was

$w + c = \frac{dx}{dt}$ , we see that  $\frac{\partial}{\partial t}(p + \rho w c) + \frac{dx}{dt} \frac{\partial}{\partial x}(p + \rho c w) = \frac{d}{dt}(p + \rho c w) = 0$  along the  $\xi = \text{constant}$

characteristics. Similarly, along the  $\eta = \text{constant}$  characteristics  $\frac{d}{dt}(p - \rho c w) = 0$  is true.

Thus we have received two ODE's which can be integrated very easily and the unknowns  $p$  and  $w$  can be computed in small time steps.

### **Initial and boundary conditions**

The importance of the type of 2<sup>nd</sup> order PDE-s lies in the fact that it determines the type of **initial and boundary conditions** assuring unique solutions.

If; for example; we prescribe for the starting time  $t = 0$  along a section of the  $x$ -axis the initial values  $p(x, t=0)$  then the function  $p(x, t)$  can be computed for the triangular region between the two characteristics  $\xi = \text{constant}$  starting from the left border and  $\eta = \text{constant}$  starting from the right border of the  $x$ -interval.

Thus if we need to get the solution over the whole pipe length  $0 \leq x \leq L$  then not only the initial  $p(x, t=0)$  distribution but also the boundary values at  $x = 0$  and at  $x = L$  must be known.

These are the boundary values

$$p(x=0, t) \quad \text{and} \quad p(x=L, t).$$

## **3. Steady flow problem leading to a hyperbolic equation**

The 2D steady isentropic flow of a compressible gas is described by the following equations ( $u, v$  denote the components of velocity vector  $\mathbf{w}$ ):

$$\text{Continuity:} \quad \frac{\partial(\rho u)}{\partial x} + \frac{\partial(\rho v)}{\partial y} = 0. \quad (7)$$

$$\text{Eulerian equations} \quad u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = -\frac{1}{\rho} \frac{\partial p}{\partial x} = -\frac{c^2}{\rho} \frac{\partial \rho}{\partial x}, \quad (8)$$

$$u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} = -\frac{1}{\rho} \frac{\partial p}{\partial y} = -\frac{c^2}{\rho} \frac{\partial \rho}{\partial y}. \quad (9)$$

Adding the  $u$ -times of Eq. (8) to the  $v$ -times of Eq. (9) and substituting Eq. (7) into the RHS of this equation one receives

$$\left(u^2 - c^2\right) \frac{\partial u}{\partial x} + \left(v^2 - c^2\right) \frac{\partial v}{\partial y} + uv \left( \frac{\partial v}{\partial x} + \frac{\partial u}{\partial y} \right) = 0. \quad (10)$$

Isentropic flow is also a vortex free flow this is a corollary of the *Crocco equation* (\*).

$$\frac{\partial u}{\partial y} - \frac{\partial v}{\partial x} = 0. \quad (11)$$

(\*) For the reversible, adiabatic case the first law of thermodynamics says  $dq = Tds = dh - \frac{dp}{\rho} = 0$ . Thus

$$\text{grad } h = \frac{1}{\rho} \text{grad } p. \text{ According to this and to Euler's equation } \text{grad} \left( \frac{\mathbf{w}^2}{2} \right) - \mathbf{w} \times \text{rot } \mathbf{w} = -\frac{1}{\rho} \text{grad } p = -\text{grad } h.$$

This gives  $\mathbf{w} \times \text{rot } \mathbf{w} = \text{grad} \left( \frac{\mathbf{w}^2}{2} + h \right) = \text{grad } h_{\dot{j}}$ . However this is zero, thus either  $\text{rot } \mathbf{w} = 0$  or  $\text{rot } \mathbf{w}$  is parallel with the velocity vector  $\mathbf{w}$  (Beltrami flow).

Now we shall define the coordinate  $x$ , the main flow direction as “time-like”. Then Eqs. (10) and (11) can be rewritten in a matrix vector formulation. Partial derivatives will be written in the short “subscript-form”.

$$\begin{pmatrix} u^2 - c^2 & uv \\ 0 & -1 \end{pmatrix} \cdot \begin{pmatrix} u_x \\ v_x \end{pmatrix} + \begin{pmatrix} uv & v^2 - c^2 \\ 1 & 0 \end{pmatrix} \cdot \begin{pmatrix} u_y \\ v_y \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \end{pmatrix}.$$

With concise notation:  $\mathbf{A}_1 \mathbf{w}_x + \mathbf{A}_2 \mathbf{w}_y = \mathbf{0}$ .

We need the earlier (\*\*\*) form thus we look for  $\mathbf{w}_x + \mathbf{A}_1^{-1} \cdot \mathbf{A}_2 \mathbf{w}_y = \mathbf{0}$ . We must find the eigenvalues of the matrix  $\mathbf{M} = \mathbf{A}_1^{-1} \cdot \mathbf{A}_2$ . Those eigenvalues will determine the slopes of characteristics running through the  $x$ - $y$  plane. The inverse of matrix  $\mathbf{A}_1$  denoted by  $\mathbf{A}_1^{-1}$  is the transposed matrix constructed from the under determinants belonging the elements of  $\mathbf{A}_1$  divided by the determinant of  $\mathbf{A}_1$ . For a 2x2 matrix it is very easy to find.  $\det \begin{pmatrix} u^2 - c^2 & uv \\ 0 & -1 \end{pmatrix} = -(u^2 - c^2)$ ,

thus  $\mathbf{A}_1^{-1} = \frac{-1}{(u^2 - c^2)} \cdot \begin{pmatrix} -1 & uv \\ 0 & u^2 - c^2 \end{pmatrix} = \begin{pmatrix} \frac{1}{u^2 - c^2} & \frac{uv}{u^2 - c^2} \\ 0 & -1 \end{pmatrix}$ . From this

$$\mathbf{M} = \mathbf{A}_1^{-1} \cdot \mathbf{A}_2 = \begin{pmatrix} \frac{1}{u^2 - c^2} & \frac{uv}{u^2 - c^2} \\ 0 & -1 \end{pmatrix} \cdot \begin{pmatrix} uv & v^2 - c^2 \\ 1 & 0 \end{pmatrix} = \begin{pmatrix} \frac{2uv}{u^2 - c^2} & \frac{v^2 - c^2}{u^2 - c^2} \\ -1 & 0 \end{pmatrix}. \quad (12)$$

The eigenvalues of matrix  $\mathbf{M}$  are solutions of  $\det(\mathbf{M} - \lambda \mathbf{E}) = 0$ . One can control that these are

$\lambda_1 = \frac{uv + \alpha c^2}{u^2 - v^2}$  and  $\lambda_2 = \frac{uv - \alpha c^2}{u^2 - v^2}$ , resp. Here  $\alpha = \frac{\text{denotes } \sqrt{u^2 + v^2 - c^2}}{c^2} \sqrt{\frac{|\mathbf{w}|^2 - c^2}{c^2}} = \sqrt{M^2 - 1}$ , where  $M$  is the local Mach-number.

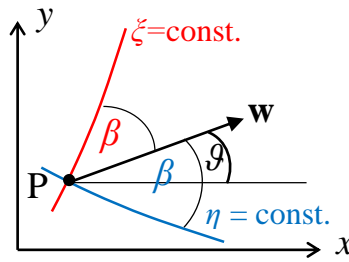
After a lengthy calculation we get an alternate form of the eigenvalues:

$$\lambda_1 = \frac{u + \alpha v}{\alpha u - v} \quad \text{and} \quad \lambda_1 = \frac{\alpha v - u}{\alpha u + v}. \quad (13)$$

With further notations  $\frac{v}{u} = \tan \vartheta$  and  $\frac{1}{\alpha} = \tan \beta$  (14)

$$\lambda_1 = \frac{\frac{1}{\alpha} + \frac{v}{u}}{1 - \frac{v}{u} \cdot \frac{1}{\alpha}} = \frac{\tan \beta + \tan \vartheta}{1 - \tan \vartheta \cdot \tan \beta} = \tan(\vartheta + \beta).$$

Thus  $\lambda_1 = \tan(\vartheta + \beta)$  and similarly  $\lambda_2 = \tan(\vartheta - \beta)$ . The slopes of characteristics is equal to the eigenvalues (see the earlier marked sentence). Now one can draw the velocity vector  $\mathbf{w}$  and the two characteristics  $\xi = \text{constant}$  and  $\eta = \text{constant}$  in the  $x$ - $y$  plane.



**Fig. 1** Characteristics  $\xi, \eta$ , velocity vector  $\mathbf{w}$ , angles  $\beta$  and  $\vartheta$

The information con of point P is bordered by the characteristic line  $\xi = \text{constant}$  and  $\eta = \text{constant}$  starting from point P. Happenings only in this region are influenced by point P. These characteristic lines are also called as Mach-lines.

### Equations to be solved along the characteristics

From  $\frac{v}{u} = \tan \vartheta$  follows  $u = w \cos \vartheta$ ;  $v = w \sin \vartheta$ . Naturally, the partial derivatives can be expressed with  $w$  and  $\vartheta$ , e.g.  $\frac{\partial u}{\partial x} = \frac{\partial w}{\partial x} \cdot \cos \vartheta - w \cdot \sin \vartheta \frac{\partial \vartheta}{\partial x}$ . Other first order derivatives have similar forms. After substituting these into Eq. (10) and rearranging we have

$$c^2 w \left( \frac{\partial \vartheta}{\partial x} \sin \vartheta - \frac{\partial \vartheta}{\partial y} \cos \vartheta \right) + (w^2 - c^2) \left( \frac{\partial w}{\partial x} \cos \vartheta + \frac{\partial w}{\partial y} \sin \vartheta \right) = 0. \quad (10a)$$

From the definition of  $\alpha, \beta$  and from the LHS formula (14)  $\sin \beta = \frac{c}{w}$ ,  $\cos \beta = \frac{\sqrt{w^2 - c^2}}{w}$ , thus

$$\cot \beta = \frac{\sqrt{w^2 - c^2}}{c} = \sqrt{M^2 - 1}. \quad \text{With all these and after dividing (10a) with } cw^2 \text{ we get:}$$

$$\sin \beta \left( \frac{\partial \vartheta}{\partial x} \sin \vartheta - \frac{\partial \vartheta}{\partial y} \cos \vartheta \right) + \frac{\cot \beta}{w} \cos \beta \left( \frac{\partial w}{\partial x} \cos \vartheta + \frac{\partial w}{\partial y} \sin \vartheta \right) = 0.$$

After a similar process the  $\cos \beta$ -times of Eq. (11) is:

$$\cos \beta \left( \frac{\partial \vartheta}{\partial x} \cos \vartheta + \frac{\partial \vartheta}{\partial y} \sin \vartheta \right) + \frac{1}{w} \cos \beta \left( \frac{\partial w}{\partial x} \sin \vartheta - \frac{\partial w}{\partial y} \cos \vartheta \right) = 0$$

Finally adding these equations (and subtracting in a second step)



$$\cos(\vartheta - \beta) \frac{\partial \vartheta}{\partial x} + \sin(\vartheta - \beta) \frac{\partial \vartheta}{\partial y} + \frac{\cot \beta}{w} \left( \cos(\vartheta - \beta) \frac{\partial w}{\partial x} + \sin(\vartheta - \beta) \frac{\partial w}{\partial y} \right) = 0, \text{ or rearranged}$$

$$\underline{\underline{\cos(\vartheta - \beta) \left( \frac{\partial \vartheta}{\partial x} + \frac{\cot \beta}{w} \frac{\partial w}{\partial x} \right) + \sin(\vartheta - \beta) \left( \frac{\partial \vartheta}{\partial y} + \frac{\cot \beta}{w} \frac{\partial w}{\partial y} \right) = 0.}} \quad (15)$$

Along the characteristics  $\eta = \text{const}$   $\lambda_2 = \tan(\vartheta - \beta) = \frac{\sin(\vartheta - \beta)}{\cos(\vartheta - \beta)} = \frac{dy}{dx} \Big|_{\eta=\text{all}}$ , so

$$\underline{\underline{\frac{\partial}{\partial \xi} = \frac{\partial}{\partial x} \cdot \frac{\partial x}{\partial \xi} \Big|_{\eta=\text{all}} + \frac{\partial}{\partial y} \cdot \frac{\partial y}{\partial \xi} \Big|_{\eta=\text{all}} = \cos(\vartheta - \beta) \cdot \frac{\partial}{\partial x} + \sin(\vartheta - \beta) \cdot \frac{\partial}{\partial y}.}}$$

If we substitute equality  $\cot \beta = \sqrt{M^2 - 1}$  into (15) we receive

$$\underline{\underline{\frac{\partial \vartheta}{\partial \xi} + \frac{\sqrt{M^2 - 1}}{w} \frac{\partial w}{\partial \xi} = 0}} \quad \text{and} \quad \underline{\underline{\frac{\partial \vartheta}{\partial \eta} - \frac{\sqrt{M^2 - 1}}{w} \frac{\partial w}{\partial \eta} = 0, \text{ resp.}}} \quad (16)$$

By the help of Fig. 2 we show how to compute intersection  $P$  of characteristics starting from points  $L$  and  $R$ :

$$\frac{y_P - y_R}{x_P - x_R} = \tan(\vartheta_R + \beta_R) \text{ and } \frac{y_P - y_L}{x_P - x_L} = \tan(\vartheta_L - \beta_L), \text{ resp.};$$

from these

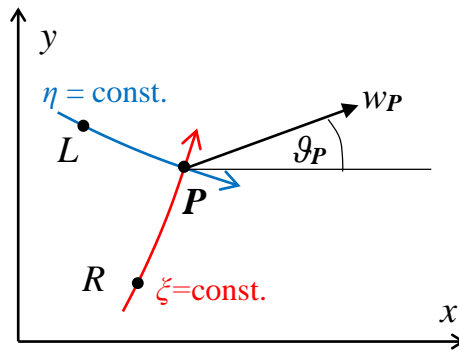
$$x_P = \frac{x_R \cdot \tan(\vartheta_R + \beta_R) - x_L \cdot \tan(\vartheta_L - \beta_L) - y_R + y_L}{\tan(\vartheta_R + \beta_R) - \tan(\vartheta_L - \beta_L)}, \text{ followed by } y_P \text{ expressed from one of the}$$

above equations.

The system of equations to be solved numerically is:

$$\underline{\underline{\vartheta_P - \vartheta_R + \sqrt{M_R^2 - 1} \frac{w_P - w_R}{w_R} = 0}} \text{ on } \underline{\underline{\xi = \text{const.}}} \text{ and } \underline{\underline{\vartheta_P - \vartheta_L + \sqrt{M_L^2 - 1} \frac{w_P - w_L}{w_L} = 0}} \text{ on } \underline{\underline{\eta = \text{const.}}}$$

lines.



**Fig. 2** Flow computation in point  $P$  from known values in points  $L$  and  $R$